

# A. Some named transport equations

Heat eqn.  $\frac{\partial T}{\partial t} = \kappa \nabla^2 T$   $\kappa [m^2 s^{-1}]$  thermal diffusivity.

in 1D  $\frac{\partial T}{\partial t} = \kappa \frac{\partial^2 T}{\partial x^2}$

What mechanisms are at work?

Hint:  $\frac{\partial \phi}{\partial t} = -\nabla \cdot \vec{F} + Q$

dimensional homogeneity requires this have unit  $m^2 s^{-1}$

$= -\frac{\partial}{\partial x} \left[ -\kappa \frac{\partial T}{\partial x} \right]$

with  $\kappa = \text{const.}$

flux divergence.  
"transport term" as has  $\nabla$  out front

where  $-\kappa \frac{\partial T}{\partial x} = F_x$  "kinematic" heat flux along  $x$  axis

Recall Fourier Law  $-\rho c_p \kappa \frac{\partial T}{\partial x} = \text{heat flux } [W m^{-2}]$   
conductive

Alternative form of the heat equation

$\rho c_p \frac{\partial T}{\partial t} = k \nabla^2 T$ ,  $k = \rho c_p \kappa$  thermal conductivity  $W m^{-1} K^{-1}$

What if problem is steady state?  $\frac{\partial T}{\partial t} = 0 = \kappa \nabla^2 T$  (2)

$\nabla^2 T = 0$  Whose equation? Laplace's equation.

$\nabla \cdot \nabla T = 0$  we now understand the "agency" at work.

$0 = \kappa \nabla^2 \phi + Q$   $\nabla^2 \phi = -Q/\kappa$  Poisson's eqn.

B. ADVECTION EQN

$\frac{\partial T}{\partial t} = -\nabla \cdot (\vec{u} T)$  kinematic convective flux of sensible heat

In 1D  $\frac{\partial T}{\partial t} = -\frac{\partial}{\partial x} (uT) \rightarrow -u \frac{\partial T}{\partial x}$  if  $u$  indep of  $x$

$\frac{\partial T}{\partial t} + u \frac{\partial T}{\partial x} = 0$  1D advection eqn with const. advective velocity.

$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} = 0$  non-linear 1D advection eqn

C. ADVECTION - DIFFUSION EQN

$$\frac{\partial \phi}{\partial t} + \vec{u} \cdot \nabla \phi = \nabla \cdot (K \nabla \phi) + Q$$

advection
diffusion  
(K may not be const.)

In atmos. sci typically the K is a molecular diffusivity and is treated as const. and the molec. term may be neglected. An exception is when the diffusion term is retained to represent "turbulent (eddy) convection".

Note that  $\vec{u} \cdot \nabla \phi = \nabla \cdot \vec{u} \phi - \phi \nabla \cdot \vec{u}$

velocity divergence, zero in some systems

It's often preferable to write the transport eqns in "flux form" ("transport form")

# WATER VAPOUR VARIABLES

$T_d$  dewpoint,  $e$  [Pa] vapour pressure (partial pressure of water vapour)

$\rho_v$  absolute humidity [ $\text{kg m}^{-3}$ ]

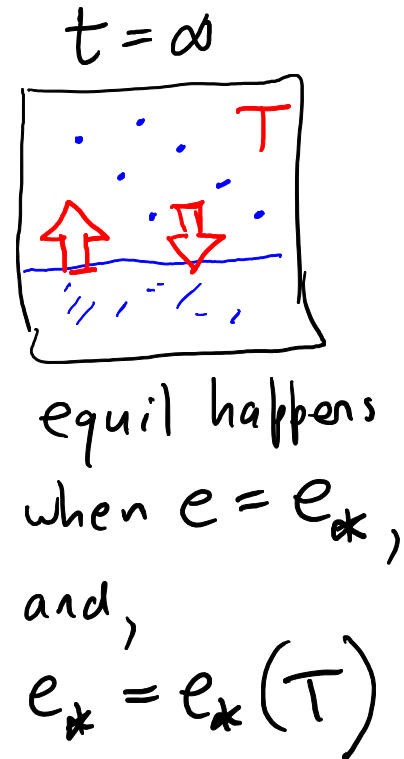
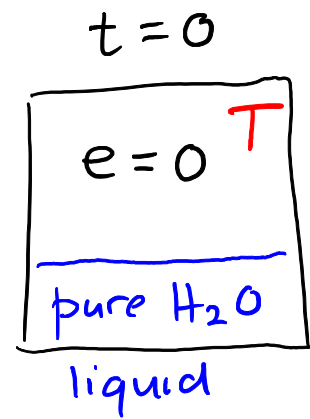
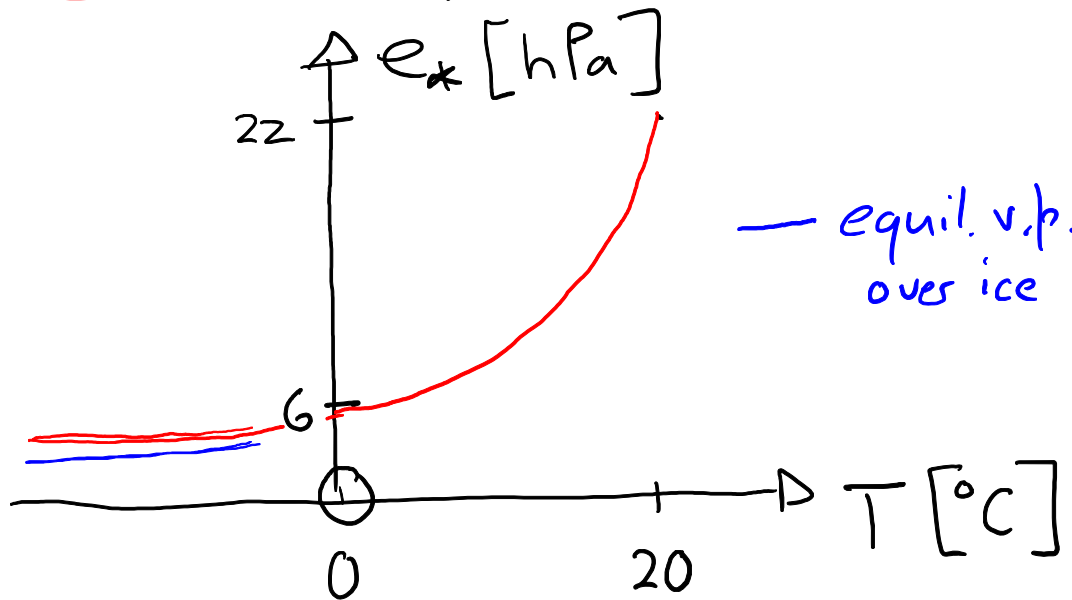
$q$  specific humidity  $q = \rho_v / (\rho_d + \rho_v)$

$r$  mixing ratio  $r = \rho_v / \rho_d$

insignificantly different for most purposes

$$RH = e / e_*(T)$$

Benchmark for vapour pressure  $e_*$



$e$  and  $T_d$  are not indep. pieces of info:

⑤

$$e = e_*(T_d) \quad RH = \frac{e_*(T_d)}{e_*(T)} \quad T \geq T_d$$

$$T_d = e_*^{-1}(e)$$

Ideal gas law for w.v.

$$e = \rho_v R_v T$$

$$R_v = 462 \text{ J kg}^{-1} \text{ K}^{-1}$$

Virtual temperature

$$T_v = T(1 + 0.61r)$$

$$P = \rho R_d T_v$$

total pressure  $\nearrow$   $\rho$   $\nearrow$  total density

$$P - e = \rho_d R_d T$$